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Mixing Flows in Dynamic Fluid Transport Simulations

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Content

- introduction
- modeling of mixing flows
- temperature modeling
- numerical experiments

Introduction

- this development is a part of our software
- in MYNTS, fluid transport modeling is based on
 - conservation of mass, molar and energy flows
 - Darcy-Weisbach pipeline pressure drop formula, with empirical friction term by Nikuradse and Hofer
 - equation of state computation by simplified analytical Papay model or more complex ISO-norm models AGA8-DC92 and GERG2008
 - customer-specific models of compressors and pumps
- this work describes in details the modeling of mixing flows and temperature in MYNTS

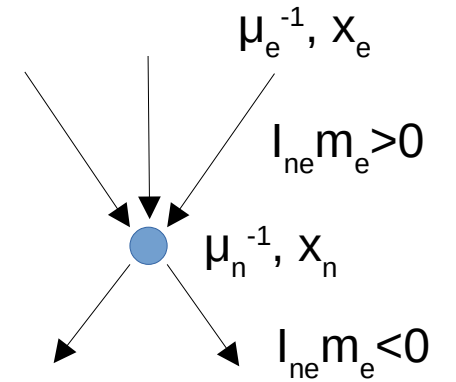
Multi-phYsics

MYNTS 

NeTwork Simulator

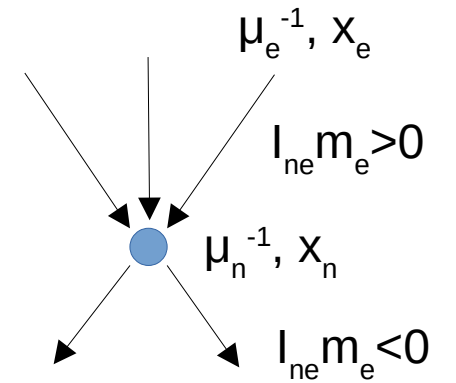
Modeling of mixing flows

- fluid transport network is a directed graph
- described by an incidence matrix I_{ne}
- each edge e has nonzero entries for the nodes n that this edge connects
 - 1 for the node that edge comes from,
 - +1 for the node that edge enters
- variables: V_n is the volume assigned to the node
- ρ_n is the mass density; m_e is the mass flow in an edge
- $\mu_{n/e}$ is the molar mass
- $x_{n/e}$ are the mole fractions of fluid components
- t is time (dynamic simulation)



Modeling of mixing flows

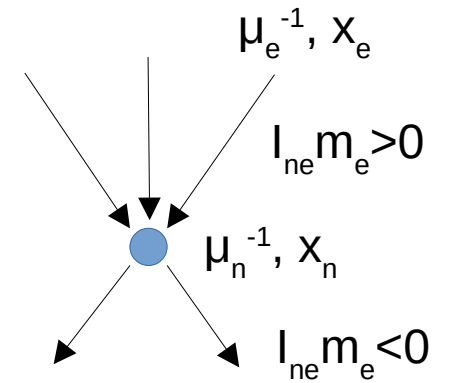
- mixing fluid flows are described by following equations
- Kirchhoff eqn: mass conservation
- mixing eqs: molar count conservation



$$V_n \partial \rho_n / \partial t = \sum_e I_{ne} m_e,$$
$$V_n \partial (\rho_n \mu_n^{-1}) / \partial t = \sum_e I_{ne} m_e \mu_e^{-1},$$
$$V_n \partial (\rho_n \mu_n^{-1} x_n) / \partial t = \sum_e I_{ne} m_e \mu_e^{-1} x_e,$$

Modeling of mixing flows

- mixing fluid flows are described by following equations



change of
mass in
the node

$$V_n \frac{\partial \rho_n}{\partial t} = \sum_e I_{ne} m_e,$$

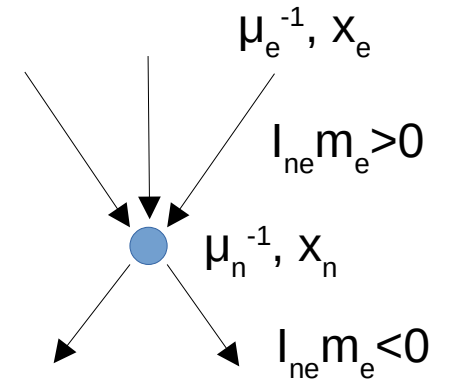
$$V_n \frac{\partial (\rho_n \mu_n^{-1})}{\partial t} = \sum_e I_{ne} m_e \mu_e^{-1},$$

mass flow
in the node

$$V_n \frac{\partial (\rho_n \mu_n^{-1} x_n)}{\partial t} = \sum_e I_{ne} m_e \mu_e^{-1} x_e,$$

Modeling of mixing flows

- mixing fluid flows are described by following equations



change of mole count in the node

$$V_n \frac{\partial \rho_n}{\partial t} = \sum_e I_{ne} m_e,$$

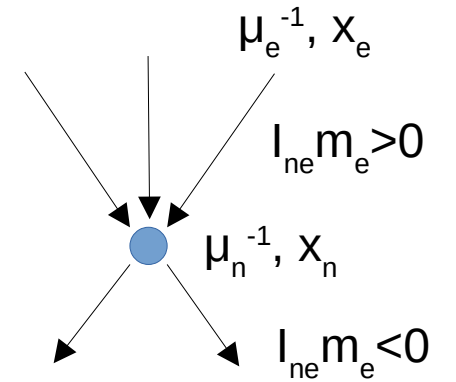
$$V_n \frac{\partial (\rho_n \mu_n^{-1})}{\partial t} = \sum_e I_{ne} m_e \mu_e^{-1},$$

$$V_n \frac{\partial (\rho_n \mu_n^{-1} x_n)}{\partial t} = \sum_e I_{ne} m_e \mu_e^{-1} x_e,$$

molar flow in the node

Modeling of mixing flows

- mixing fluid flows are described by following equations



change of
component
mole count
in the node

$$V_n \partial \rho_n / \partial t = \sum_e I_{ne} m_e,$$

$$V_n \partial (\rho_n \mu_n^{-1}) / \partial t = \sum_e I_{ne} m_e \mu_e^{-1},$$

$$V_n \partial (\rho_n \mu_n^{-1} x_n) / \partial t = \sum_e I_{ne} m_e \mu_e^{-1} x_e,$$

component
molar flow
in the node

Modeling of mixing flows

- more convenient form, resolved with respect to derivatives

$$\begin{aligned}V_n \rho_n \partial \mu_n^{-1} / \partial t &= \sum'_e I_{ne} m_e (\mu_e^{-1} - \mu_n^{-1}), \\V_n \rho_n \mu_n^{-1} \partial x_n / \partial t &= \sum'_e I_{ne} m_e \mu_e^{-1} (x_e - x_n), \\ \sum'_e &= \sum_{e, I_{ne} m_e > 0},\end{aligned}$$

- boundary conditions in entry nodes: $\mu = \mu_{\text{set}}$, $x = x_{\text{set}}$
- startup: zero massflows, all eqs initially satisfied

Temperature modeling

- variables: U is the molar internal energy
- $H = U + P \mu/\rho$ is the molar enthalpy, P is the pressure
- equations: energy conservation for open systems

change of
internal
energy
in the node

$$\rightarrow \boxed{V_n \partial(\rho_n \mu_n^{-1} U_n) / \partial t} = \sum_e \boxed{I_{ne} m_e \mu_e^{-1} H_e}, \leftarrow$$

flow of
enthalpy
in the node

includes work of
pressure force at
the boundary

Temperature modeling

$$V_n \rho_n \mu_n^{-1} \partial H_n / \partial t - V_n \partial P_n / \partial t = \\ = \sum_e' I_{ne} m_e \mu_e^{-1} (H_e - H_n),$$

- more convenient form
- boundary conditions in entry nodes: $H = H_{\text{set}}$, or $T = T_{\text{set}}$
- gravitational and kinetic terms: $H \rightarrow H + \mu g h + \mu v^2 / 2$, where g is the acceleration of free fall, h is the height, and v is the speed of the fluid

- HT -constraint:
$$H = H_{\text{mod}}(P, T, x), \quad (\text{exact})$$

$$H = H_{\text{mod}}(P, T_{\text{prev}}, x) + c_p (T - T_{\text{prev}}), \quad (\text{linearized})$$

- H_{mod} is the thermodynamic model for enthalpy,
 $c_p = \partial H_{\text{mod}} / \partial T$ is the molar heat capacity

Temperature modeling

- ISO norm GERG2008 used as thermodynamic model
- linearized eqn makes mixing subsystem linear at each iteration step
- other equations
- default element equation (transport of enthalpy)
- applicable to valves, regulators, resistors and shortcuts

$$H_e = m_e > 0? H_{n1} : H_{n2}$$

Temperature modeling

- pipe equation: $(m_e > 0? (H_{n1} - H_e)\mu_{n1}^{-1} : (H_{n2} - H_e)\mu_{n2}^{-1}) |m_e| = \pi D L c_{ht} (T_e - T_{soil}),$
- describes heat exchange with soil: T_{soil} is soil temperature, D is pipe diameter, L is pipe length, c_{ht} is heat transfer coefficient
- compressor equation: $m_e > 0? (T_e - T_{n1} ((|P_{n2}/P_{n1}|^{(\kappa-1)/\kappa} - 1)/\eta + 1) z_{n1}/z_e) : (H_e - H_{n2}) = 0,$
- describes isentropic compression: κ is isentropic exponent, η is isentropic efficiency, z is compressibility factor

Temperature modeling

- coolers and heaters:

$$m_e > 0 ? (A_{set} > 0 ? (T_e - T_{set}) : (H_e - H_{n1})) \\ : (H_e - H_{n2}) = 0,$$

- is a linearization of clamp formulas: $T_e = \min(T_{n1}, T_{set})$ for coolers and $T_e = \max(T_{n1}, T_{set})$ for heaters

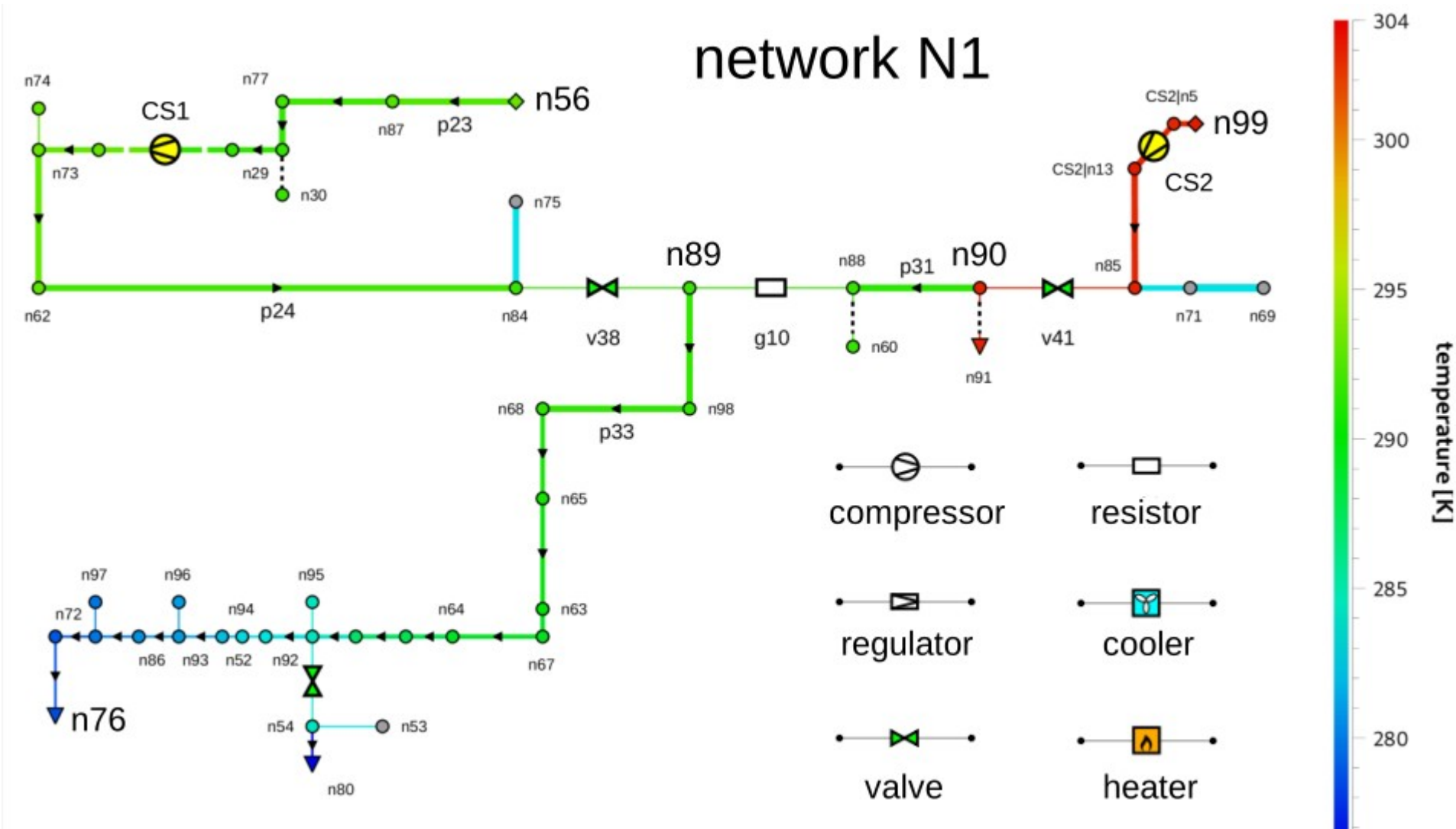
Algorithm (active set):

cooler: if(Aset==1&&He>Hn1) then Aset=0; if(Aset==0&&Te>Tset) then Aset=1

heater: if(Aset==1&&He<Hn1) then Aset=0; if(Aset==0&&Te<Tset) then Aset=1

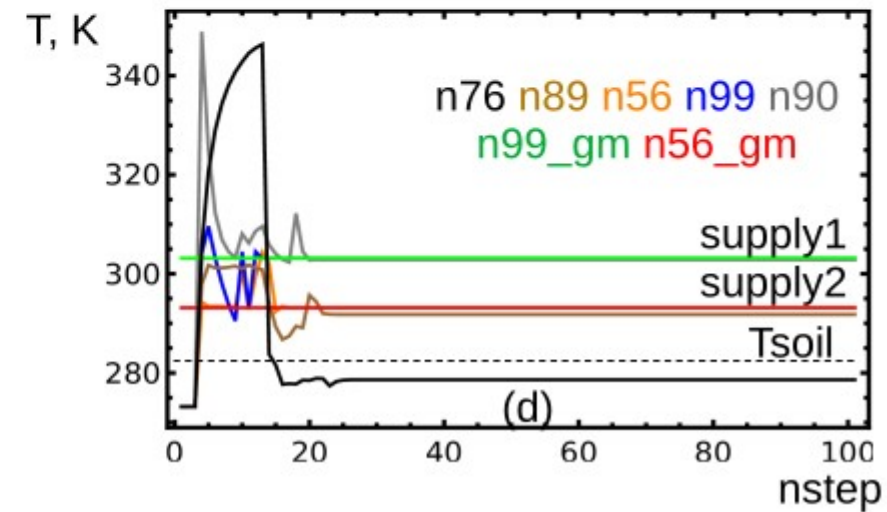
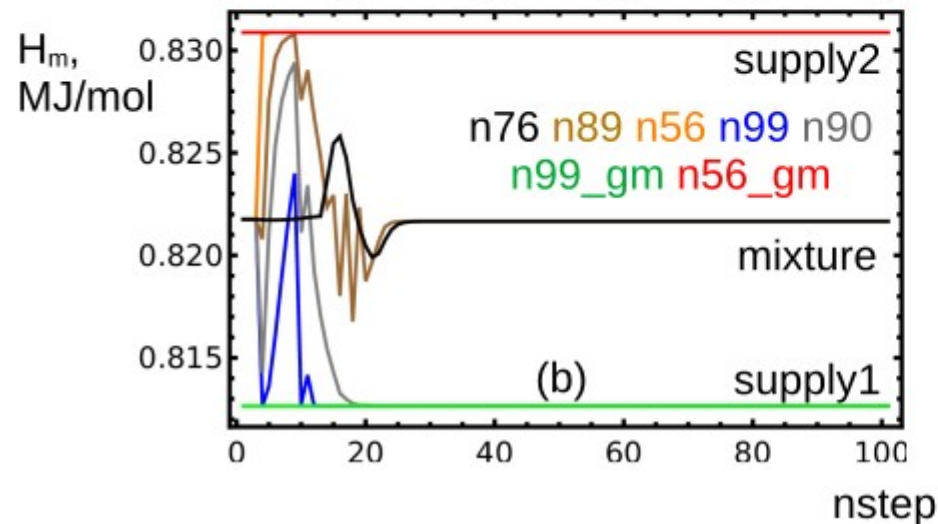
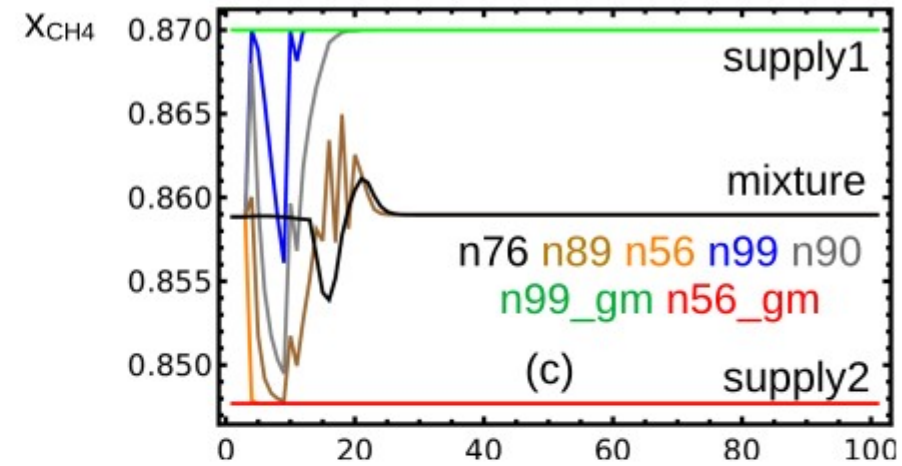
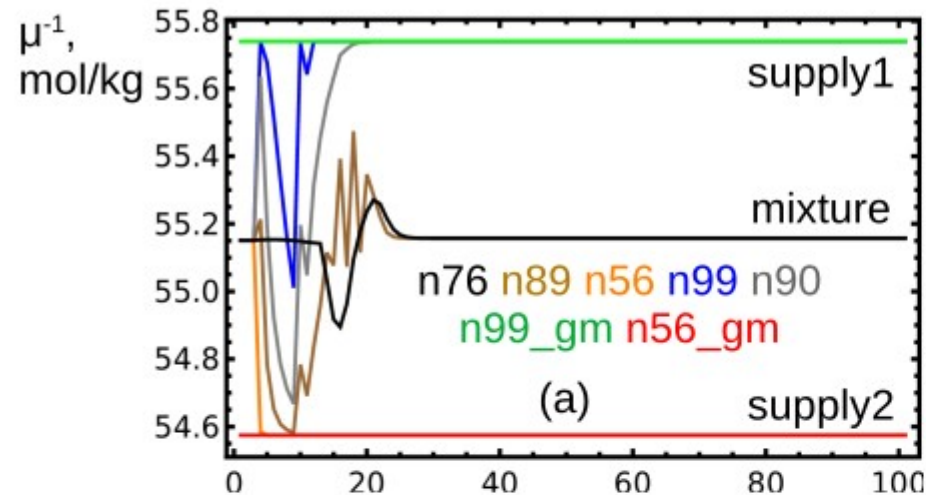
Numerical experiments

- test network
- 100 nodes
- 111 edges
- 2 entries
- 3 exits
- 4 compressors in 2 stations
- filled with nat.gas



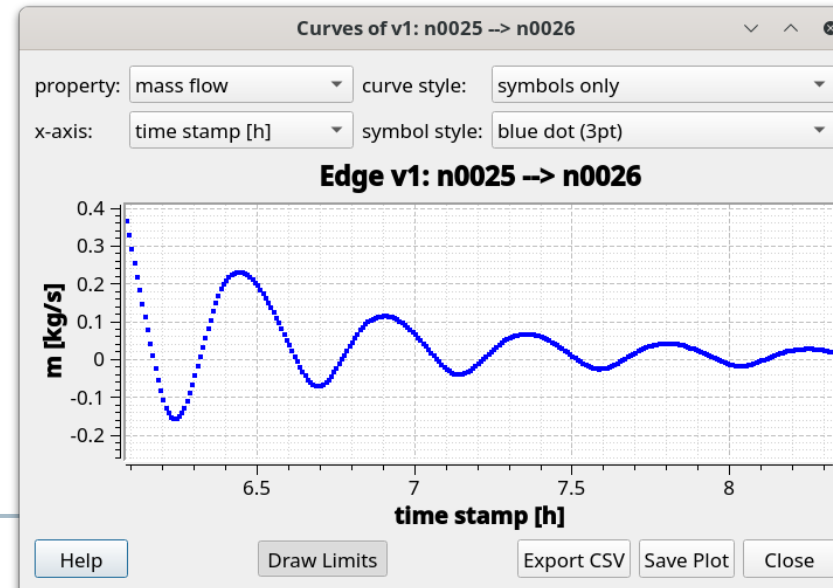
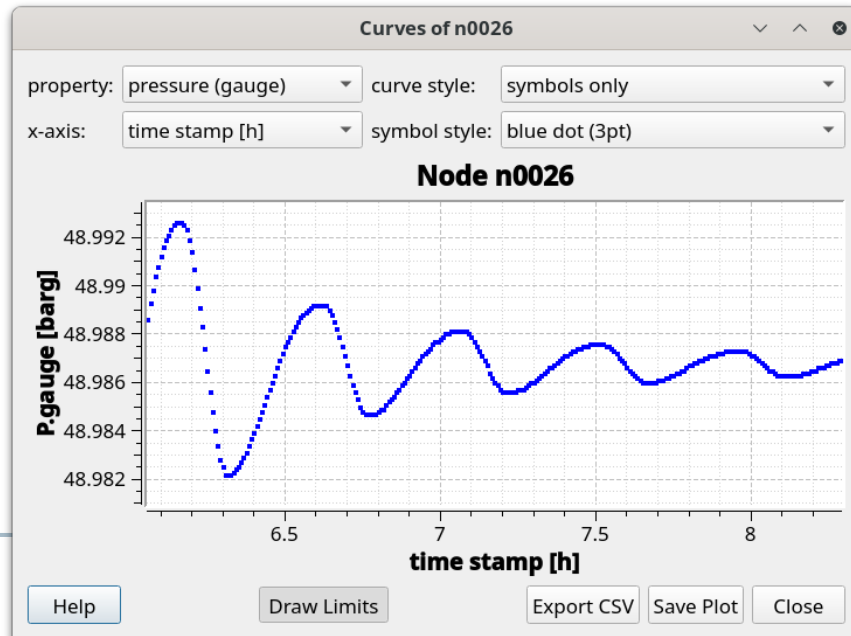
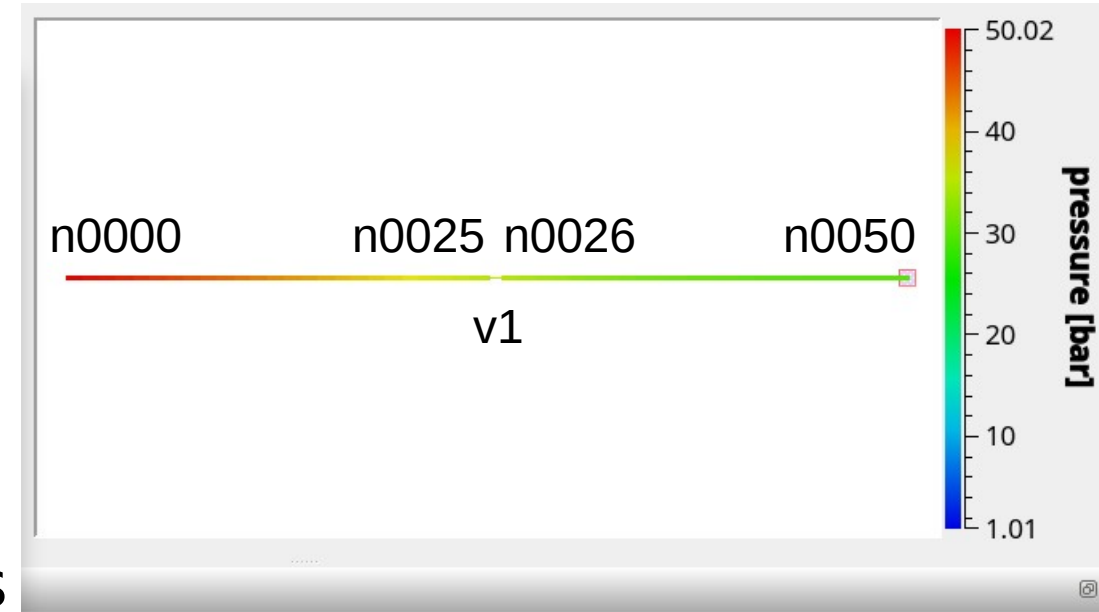
Numerical experiments

- evolution of
- (a) inverse molar mass
- (b) combustion heat value
- (c) methane fraction
- (d) absolute temperature



Numerical experiments

- hydrogen and carbon dioxide pipelines
- $L = 150\text{km}$ $D = 0.5\text{m}$ $n_{\text{subdiv}} = 50$
- one valve inbetween
- used for testing of the temperature modeling and simulation of shockwaves



Conclusion

- this work presents a new numerically efficient implementation of flow mixing algorithms in dynamic simulation of pipeline fluid transport
- mixed characteristics include molar mass, heat value, chemical composition and the temperature of the transported fluids
- in the absence of chemical reactions, the modeling is based on the universal conservation laws for molar flows and total energy
- the modeling formulates a sequence of linear systems, solved by a sparse linear solver, typically in one iteration per integration step
- the functionality and stability of the developed simulation methods have been tested on a number of realistic network scenarios

Thank you for your
attention
